#### Residual stress caused by heat treatments of Steel and Aluminum alloy castings

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# Outline

#### 1. Introduction to residual stress

- Effect of thermal gradient
- Effect of phase transformation
- Effect of casting geometry
- 2. Objective
- 3. Consequences of the residual stress
- 4. Case histories:
  - #1 Distortion during solidification (steel casting)
  - #2 Fracture during field working (steel casting)
  - #3 Fracture during heat treatment (steel casting)
  - #4 Distortion during heat treatment (aluminum casting)

 Metallic parts present thermal expansion during heating operations and thermal contraction during cooling operations;



- Thermal Gradients promotes residual stress
- At high temperature residual stress are relived
- Most of residual stresses are generated during cooling operations;



Simulation of Heat Treatment Distortion - R.A. Hardin1and C. Beckermann – Proceedings of the 59<sup>th</sup> SFSA Technical and Operational Conference – Paper #33, 2005.

![](_page_6_Picture_1.jpeg)

Part at homogeneous temperature

![](_page_7_Picture_1.jpeg)

Part at homogeneous temperature Surface contraction restricted by the core (surface with tensile residual stress)

![](_page_8_Picture_1.jpeg)

Part at homogeneous temperature

Surface contraction restricted by the core

Surface with tensile residual stress

Core contraction restricted by the surface

Surface with compressive residual stress

![](_page_9_Figure_1.jpeg)

Simulation of Heat Treatment Distortion - R.A. Hardin1and C. Beckermann – Proceedings of the 59<sup>th</sup> SFSA Technical and Operational Conference – Paper #33, 2005.

- Compressive stresses in the surface of the casting are considered positive, since these stresses can minimize the possibility of crack formation;
- On the other hand, tensile stresses in the surface of a casting can promote distortion or can contribute to crack initiation;

#### Introduction to residual stress Effect of thermal gradient

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#### Introduction to residual stress Effect of thermal gradient

![](_page_12_Figure_1.jpeg)

Simulation of Heat Treatment Distortion - R.A. Hardin1and C. Beckermann – Proceedings of the 59<sup>th</sup> SFSA Technical and Operational Conference – Paper #33, 2005.

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![](_page_14_Figure_1.jpeg)

![](_page_15_Figure_1.jpeg)

Failures Related to Heat Treating Operations - G.E. Totten, G.E. Totten & Associates, Inc. M. Narazaki, Utsunomia University (Japan) R.R. Blackwood, Tenaxol Inc.

![](_page_16_Figure_1.jpeg)

![](_page_17_Figure_1.jpeg)

during

![](_page_19_Picture_1.jpeg)

Temperature

![](_page_20_Figure_1.jpeg)

![](_page_21_Figure_1.jpeg)

![](_page_22_Figure_1.jpeg)

Volumetric

contraction

during

cooling

![](_page_23_Picture_1.jpeg)

#### Temperature

![](_page_24_Picture_0.jpeg)

![](_page_25_Picture_0.jpeg)

The main objective of the article is to evaluate the reliability of the MAGMASOFT Stress Simulation to explain some distortion and breakage problems of Steel and Aluminum alloy castings;

 A second objective is to use the simulation tool to adjust the production process in order to minimize these problems;

# **Consequences of the residual stress**

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The main consequences of the tensile residual stresses are casting distortion and casting breakage;

# **Consequences of the residual stress**

•Value of the tensile residual stresses:

- Stresses < YS Contribution to distortion or breakage in field application;
- Stresses > YS Distortion during manufacture and can break in the field;
- Stresses > UTS Fracture during the manufacture;

![](_page_30_Picture_1.jpeg)

#### Grate Liner for SAG Mill

#### Part weight: 2670 kg

Alloy: Cr-Mo Pearlitic low alloy steel

![](_page_31_Picture_1.jpeg)

#### Grate Liner for SAG Mill

eso: 942 kg

![](_page_32_Picture_1.jpeg)

# Crack position at the end of Normalizing heat treatment (still air cooling)

![](_page_33_Picture_1.jpeg)

# Crack position at the end of Normalizing heat treatment (still air cooling)

![](_page_34_Picture_1.jpeg)

# Crack position at the end of Normalizing heat treatment (still air cooling)

![](_page_35_Picture_1.jpeg)

Failure analysis - Crack position with lateral displacement of the material

![](_page_36_Picture_1.jpeg)

Failure analysis – Fracture surface without oxidation (low temperature) and evident Chevron marks.

![](_page_37_Picture_1.jpeg)

Failure analysis – Fracture surface without oxidation (low temperature) and evident Chevron marks showing the fracture propagation direction.

![](_page_38_Picture_1.jpeg)

Fracture mechanism – The thin sections B are the first to transform in Pearlite with free expansion. When section C transform in Pearlite, the correspondent expansion displace the lateral bar left and imposes tensile stress in the B section which is restricted by the thick A section, promoting the crack.

![](_page_39_Figure_1.jpeg)

Typical temperature curves variation from thin and thick regions of the casting during the normalizing heat treatment.

![](_page_40_Figure_1.jpeg)

Result of the stress simulation after the normalizing heat treatment: the maximum stress level is around 700 MPa and the UTS is around 700 MPa.

![](_page_41_Picture_1.jpeg)

Result of the stress simulation after the normalizing heat treatment: the maximum stress level is around 700 MPa and the UTS is around 700 MPa.

- The maximum level of residual stress formed due to the normalizing heat treatment are around 700 MPa and the ultimate tensile strength of the low alloy steel is also around 700 MPa, so the residual stress should explain the fractures after normalizing heat treatment;
- Aiming to reduce the crack formation, the heat treatment was adjusted using the stress relieved immediately after normalizing heat treatment.

![](_page_43_Figure_1.jpeg)

Typical temperature curves variation from thin and thick regions of the casting during the normalizing and stress relieve heat treatment.

![](_page_44_Figure_1.jpeg)

Result of the stress simulation after the normalizing and stress relieve heat treatment: the maximum stress level was reduced to around 100 MPa.

![](_page_45_Figure_1.jpeg)

Result of the stress simulation after the normalizing and stress relieve heat treatment: the maximum stress level was reduced to around 100 MPa.

- The maximum level of residual stress formed due to the normalizing heat treatment are around 700 MPa and the ultimate tensile strength of the low alloy steel is also around 700 MPa, so the residual stress should explain the fractures after normalizing heat treatment;
- Using the stress relieve heat treatment immediately after normalizing the residual stress level was reduced to around 100 MPa.

![](_page_48_Picture_1.jpeg)

![](_page_48_Picture_2.jpeg)

Flywheel housing for diesel engine

# Alloy: A356 T6 aluminum alloy

![](_page_49_Figure_1.jpeg)

# Yield strength values in the as cast condition estimated by simulation (minimum value around 120 MPa)

![](_page_50_Figure_1.jpeg)

Description of the T6 heat treatment using a quench in water after the solution cycle which imposes residual stress.

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Critical step to residual stress is water quench

Typical YS during quenching = 120 MPa

![](_page_52_Figure_1.jpeg)

#### Maximum residual stress level is over YS and near the UTS value HIGH PROBABILITY OF DISTORTION

![](_page_53_Figure_1.jpeg)

Reduction of around 20% of the residual stresses level with increasing the water temperature from 25 to 75 C.

![](_page_54_Figure_1.jpeg)

Final stress level after complete heat treatment estimated by stress simulation (residual stress level of 105 MPa compromises almost 50% of the YS)

- Water temperature has a little effect on residual stress
- in order to reduce distortion = casting design adjustment

![](_page_56_Picture_0.jpeg)